



# *WGCMA FLOODPLAIN MAPPING PROGRAM*

**OFFICIAL** 

# **Floodplain mapping for Glengarry/Eaglehawk Creek**

**August 2023**



# <span id="page-1-0"></span>**DOCUMENT DETAILS**





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# <span id="page-9-0"></span>**SECTION A INTRODUCTION**

# <span id="page-9-1"></span>**1 PURPOSE**

This study is an update of the existing flood information produced in 2015 as part of the Student Floodplain Mapping Program run by the West Gippsland Catchment Management Authority. The 2015 flood study of the Eaglehawk Creek had a number of issues with it that needed to be resolved.

The focus area for this study are the waterways Eaglehawk Creek and Four Mile Creek and covers the township of Glengarry and surrounding rural areas.

# <span id="page-9-2"></span>**2 OBJECTIVE**

This flood study seeks to produce detailed flood mapping for the township of Glengarry and surrounding rural areas.

This flood study will produce results for;

- Flood Extent
- Flood water depth
- Flood water velocity
- Water surface elevation

These results will cover the design flood events of 20%, 10%, 5%, 2% and 1% AEP.

The results of this study transition into the 2015 Latrobe River Flood Study by Cardno overlapping at the downstream of this study area.

The information presented in this report has been compiled for use by West Gippsland Catchment Management Authority (WGCMA) for statutory planning, community education/preparedness, flood risk for insurance purposes and emergency management purposes.

The study has been completed in accordance with the guidance provided in AR&R 2019. As such, this study represents the best available flood risk information for this area.

# <span id="page-10-0"></span>**3 CATCHMENT DESCRIPTION**

The Eaglehawk Creek Catchment is predominantly rural, covering an area of approximately 129 square kilometres. The most upstream section of the catchment runs along the Cowwarr-Walhalla Road and the catchment finishes at the inflow of the Eaglehawk and Four Mile Creek into the Latrobe River (refer to [Figure 1](#page-11-0) for a map detailing the Eaglehawk Creek Catchment).

In terms of topography, the Traralgon Creek catchment rises to 405 metres AHD down to 20 metres AHD at the confluence with the Latrobe River. Rainfall across this catchment differs significantly across the catchment in most rainfall events, with a majority of the rainfall falling in the north of the catchment in the hills.

The channels and tributaries within the North half of the catchment are all well-defined, due to the steep elevation and grade of the terrain. The primary land use of this portion of the catchment is tree plantations, whereas the northern half of the catchment is primarily flat floodplains which is used primarily for farming.



<span id="page-11-0"></span>**Figure 1 Eaglehawk Creek Catchment**

# <span id="page-12-0"></span>**4 FLOOD DATA REVIEW**

### <span id="page-12-1"></span>**4.1 Flow and rainfall gauge data**

As part of the initial desktop analysis, an investigation into the availability of the flow gauges was performed. There are no flow gauges on the Eaglehawk Creek, so therefore a detailed calibration of the hydrology is not possible at this time.

### <span id="page-13-0"></span>**4.2 Previous decision-related data**

[Figure 2](#page-13-1) shows the previous decision-related flood information for this area. It has been coloured by the different reliability ratings. As seen in [Figure 2,](#page-13-1) the reliability for the previous flood information for Eaglehawk Creek was deemed to be medium in reliability, however a review of the data has since been completed and found issues with the previous mapping of the Eaglehawk Creek and found it to be low in reliability.

<span id="page-13-1"></span>

**Figure 2 Previous Decision Related Data**

# <span id="page-14-0"></span>**SECTION B HYDROLOGY**

The hydrology component of this study was used to estimate the amount of flow produced across the catchment during different sized events. These flows were then used as inputs in the hydraulic component of the study.

There were three different hydrology approaches that were adopted as part of the hydrology modelling processes, these were;

- Flood frequency analysis using the ARR's online RFFE Model (Commonwealth of Australia: Engineers Australia, n.d.)
- Hydrology modelling using RORB

The RORB hydrology model was used to produce hydrographs at key locations across the catchment. The RORB model was developed in accordance with best practice from the data from the ARR Datahub and BOM IFD and verified to align with the results from and RFFE Model results.

# <span id="page-14-1"></span>**1 CATCHMENT DELINEATION**

The first stage of the flood study was to define the catchment area of Eaglehawk Creek that will be modelled as part of this study. The catchment of the Eaglehawk Creek was defined using the following sets of data.

### <span id="page-14-2"></span>**1.1 Aerial photography**

There are several different datasets for aerial photography available to the WGCMA for this area. These datasets and their corresponding date flown, and resolution have been listed in [Table 1.](#page-14-3) Where possible, the datasets that were the most recent and with the highest resolution were used in preference.

#### <span id="page-14-3"></span>**Table 1 Available data - Aerial photography**



These datasets were used in combination with the elevation data and waterways and catchment mapping layers to digitise the reaches and subareas for this catchment model.

### <span id="page-15-0"></span>**1.2 Elevation data**

There were three different elevation datasets that were used for this study, the details of these can be found in [Table 2.](#page-15-1)

<b>Dataset</b> <b>Name</b>	<b>Date</b>	<b>Resolution</b>	<b>Vertical Accuracy</b>	<b>Horizontal Accuracy</b>
<b>West</b> Gippsland Riparian	September 2011	1 metre	at 67% 0.19 metre Confidence Interval	78% 0.2 metre at Confidence Interval
<b>West</b> <b>Gippsland</b> <b>Floodplain</b>	February 2011	1 metre	Target 0.10m at 67 % Confidence Interval	Actual 0.19m at 67 % Confidence Interval
<b>Vicmap</b> <b>Elevation</b> DTM 10m	1974 2006	10 metres	5 metres	12.5 metre

<span id="page-15-1"></span>**Table 2 Available data - Elevation data**

As seen in [Table 2,](#page-15-1) the West Gippsland Riparian and the West Gippsland Floodplain datasets are significantly more accurate and has a much higher resolution than the VicMap DTM. The limitation of these more accurate datasets is that these datasets only cover the floodplain of the Eaglehawk and Four Mile Creek, whereas the VicMap DTM has complete coverage of the Catchment. The extents of these different layers can be seen in [Figure 3.](#page-16-0) When formulating the subareas for the catchment file, the VicMap DTM was the primary source of information, due to the VicMap DTM's coverage.

Another component important consideration when defining the catchment file for the RORB model is the extent of the hydraulic model. Due to constraints regarding grid resolution and accuracy, the hydraulic model did not use the VicMap DTM and was limited to the coverage of the West Gippsland Riparian and Floodplain datasets. The RORB hydrology model needed to meet the recommendations stated within the RORB manual, which is that there needs to be at least 5 sub-areas upstream of the intersection between a RORB reach and the hydraulic model boundary (Laurenson, Mein, & Nathan, 2010).

The above considerations were used in combination with the aerial imagery, waterway layers and catchment mapping layers to digitize the reaches and subareas for this catchment model.

<span id="page-16-0"></span>

**Figure 3 Available Data - Elevation Data**

### <span id="page-17-0"></span>**1.3 Catchment area**



[Figure 4](#page-17-1) shows the catchment area defined by this flood study.

<span id="page-17-1"></span>**Figure 4 Traralgon Creek Catchment Area**

# <span id="page-18-0"></span>**2 RORB HYDROLOGIC MODEL**

RORB is the standard hydrology model used by the West Gippsland Catchment Management Authority (WGCMA). It is an interactive runoff and streamflow routing program (Laurenson, Mein, & Nathan, 2010) and has traditionally been used by the WGCMA to calculate streamflow hydrographs at location within a stream from rainfall events. These hydrographs are usually input into a hydraulic model (e.g. TUFLOW) to represent the rainfall occurring within the catchment during a specific AEP event.

### <span id="page-18-1"></span>**2.1 Sub-area and reach delineation**

The catchment file for RORB was set up using HARC's ArcRORB tool. The sub-areas and reaches were defined from the elevation data sets.

The sub areas were delineated in a way to ensure that all print nodes intended to be used to generate hydrographs for TUFLOW had at least 5 subareas upstream of any nodes that results are required (Laurenson, Mein, & Nathan, 2010).

The Vicmap DTM was once again the primary elevation dataset used to delineate the subareas and reaches.



<span id="page-19-0"></span>**Figure 5 RORB Hydrology Model**

### <span id="page-20-0"></span>**2.2 Initial Parameters**

#### <span id="page-20-1"></span> $2.2.1$ *Storm loss parameters*

The initial parameters that were used were based off values given from the Australian Rainfall & Runoff's Data Hub (Ball, et al., 2016). The catchment data from coordinates of 146.53 longitude and -38.08 latitude were inputted into the Data Hub (location shown in [Figure 6\)](#page-20-3) on the 9<sup>th</sup> of February 2021.

The Data Hub prescribed a Storm Initial Loss of **25.0** millimeters and a Storm Continuing Loss of **3.6** millimeters.



<span id="page-20-3"></span>**Figure 6 Map from the ARR Datahub showing catchment centroid**

#### <span id="page-20-2"></span> $2.2.2$ *Kc*

Kc is a flow routing parameter used by RORB, kc is an empirical coefficient applicable to the catchment (or, more rarely, a subcatchment) and stream network, (Laurenson, Mein, & Nathan, 2010). This parameter effects the time it takes for the water to move through the catchment model.

The initial estimates for kc, were based on the regional estimation equations in ARR2016.

The guidelines suggested by the 2016 ARR for the eastern parts of Victoria is that the Vic (MAR>800mm) equation is a suitable equation for working out the Kc of the catchment, MAR being the mean annual rainfall for the catchment (Book 7 Chapter 6 6.2.1.3 ARR 2016).

Recommendations from HARC is that the Pearse equation is more suitable for this application as it takes into consideration the average distance from sub-area centroid to outlet in its calculations (Stephens, 2019).

The adopted kc parameter for this model was 17.47 based on the Pearse equation.

#### <span id="page-21-0"></span> $2.2.3$ *m*

The industry standard for the non-linearity parameter (m) is 0.8 (Book 7 Chapter 6.2 ARR 2016). There was not adequate data provided to indicate that the m value should be adjusted from this industry standard, therefore the value for m used for RORB was 0.8.

### <span id="page-22-0"></span>**2.3 Monte-Carlo**

The use of Monte-Carlo modelling follows the ARR's recommendation for reducing any bias of estimated flood probabilities (Nathan & Ling, 2016). In a Monte Carlo simulation, influential modelling parameters are stochastically varied across each run. For Eaglehawk Creek, 10,000 individual runs are performed during each simulation.

Rather than outputting a series of hydrographs, the Monte Carlo simulation outputs just the peak flows of each of the 10,000 individual runs along with the parameters used to create them, forming a flood frequency curve.

This process was used to identify the critical storm parameters for each event size, these parameters included:

- Critical storm duration.
- Temporal pattern shape.
- Continuous loss percentage.

#### <span id="page-22-1"></span> $2.3.1$ *Input Data*

The following sections present the alternative data that is used during the design run stages of the RORB hydrology modelling.

#### <span id="page-23-0"></span>2.3.1.1 Intensity Frequency Duration tables

The Intensity Frequency Duration (IFD) tables were used by RORB to define the total amount of rainfall depth expected during an event of a certain size and duration.

The IFD table that was used as part of this study has been displayed in [Table 3.](#page-23-2) The left column relates to the total duration of the rainfall event, the top row is the size or AEP % of the rainfall event and the remaining numbers are the depth of rainfall expected for a rainfall event of a given duration and event.



<span id="page-23-2"></span>

#### <span id="page-23-1"></span>2.3.1.2 Temporal Patterns

A temporal pattern is a unit hyetograph which is used by RORB to temporally vary the rainfall input into a hydrology model.

The temporal pattern was used to multiply each percentage increment in the temporal pattern by the total storm intensity specified by the IFD table across the duration of the storm, giving a hyetograph.

The 2016 ARR guidelines recommends that at a minimum 10 temporal patterns are ran through a hydrology model and the most suitable of the 10 be selected for use within the design runs. The set 10 temporal patterns have been supplied by the ARR via the ARR datahub (Babister, Trim, & Retallick, 2017).

These temporal patterns can be found in the ARR datahub website.

#### <span id="page-24-0"></span>2.3.1.3 Areal Reduction Factors

The Areal Reduction Factor (ARF) is another parameter that comes from the Data Hub. The ARF value that was used was based off the area of the entire catchment to the outlet. Well into the hydraulic modelling phase, advice from Hydrology and Risk Consulting (HARC) was delivered around the ARF factor. This advice was that the ARF should be calculated based off stream length and catchment areas to each print node, rather than the outlet (Stephens, 2019). In order to have each printed hydrograph feature a correct ARF, a new model would need to be ran for each print node that would require a different ARF value. This will process will be amended for future studies, but this advice was given after the modelling had been completed and was too late in the modelling process to be implemented.

### <span id="page-24-1"></span>**2.4 Design run**

<span id="page-24-2"></span>The purpose of the design run stage is to produce hydrographs at key locations throughout the catchment, (shown further in the report in [Figure 8\)](#page-30-0). The design run stage uses the same input data as the validation stage. However, rather than running a Monte Carlo suite of varying parameters, the Design run stage only runs a singular storm event for each AEP. Results

### <span id="page-25-0"></span>**2.5 Assumptions**

#### <span id="page-25-1"></span> $2.5.1$ *Validation stage using the Monte Carlo*

Much like when performing a flood frequency analysis of gauged results, RORB's Monte Carlo analysis only looks at the peak flow of each of the hydrographs produced during a simulated storm to calculate the storms AEP. The issue with this approach is that it does not take into account the overall shape of the hydrograph and favours hydrographs that are more peaked in shape.

In addition to this, analysis during the validation really should be conducted at a larger number of print locations rather than just at the outlet or gauge locations in order to find a design storm that causes the desired AEP across locations across the entirety of the catchment.

#### <span id="page-25-2"></span> $252$ *Delineation of the catchment*

In order to meet recommendations around the size of subareas and the 5 subareas above a print location, a number of potential flow paths were not included in the RORB model. While these missed flow paths are unlikely to significantly affect the flooding of the Traralgon Creek, some localised inundation may have been missed.

# <span id="page-26-0"></span>**SECTION C HYDRAULICS**

# <span id="page-26-1"></span>**1 DESCRIPTION OF HYDRAULIC MODELLING APPROACH ADOPTED**

The hydraulic analysis of Eaglehawk Creek was performed through a hydraulic modelling program called TUFLOW. TUFLOW used the hydrographs produced by RORB as flow inputs into the hydraulic model. The hydraulic model of Eaglehawk Creek is primarily 2D (2- Dimensional), with only a few 1D (1-Dimensional) networks which model the more significant hydraulic structures within the system. The choice to use 2D for this model was made as generally it is quicker and more advantageous to set up a 2D model than a 1D/2D hybrid. The 2D model components consists of a 2-metre grid DEM representing elevation for Eaglehawk Creek.

Aerial photography was used to identify any hydraulic features of significance within the model extent and model these features either as hydraulic structures such as culverts, or simply as areas of increased roughness. The aerial photography was also used to check LiDAR data for any inaccuracies or errors.

# <span id="page-26-2"></span>**2 AVAILABLE DATA**

### <span id="page-26-3"></span>**2.1 Aerial photography**

The aerial photography was used primarily to define the different materials within the floodplain and to identify hydraulic structures that needed further investigation.

In addition, the aerial imagery helped identify defects within the lidar datasets, as it was able to confirm whether the presence of dense vegetation, fences or other features had possible been picked up.

### <span id="page-26-4"></span>**2.2 Elevation data**

For this component of the study, the primary concerns with the elevation datasets were the accuracy and resolution of the elevation dataset. The coverage of the elevation was less of a concern, as the hydraulic extent needed to be reduced to aid in run time anyway.

As shown in [Figure 3,](#page-16-0) the Riparian and Floodplain dataset are generally limited to the floodplain area of the Eaglehawk Creek.

### <span id="page-27-0"></span>**2.3 VicMap data**

#### <span id="page-27-1"></span> $2.3.1$ *Roads*

Information around the location of roads was primarily from the Road Network – Vicmap Transport layer. The roads layer was used to define the location of where road material roughness should be applied.

#### <span id="page-27-2"></span> $2.3.2$ *Land-zoning*

The Vicmap Planning layers were used to determine the land usage of each of the lots and was used in conjunction with the available areal imagery to delineate the material layer across the catchment. While the Vicmap Planning layer was a good start, due to the majority of the catchments land zone being FZ, the imagery and lidar datasets where still required for much of the roughness defining process.

# <span id="page-27-3"></span>**3 CATCHMENT EXTENT HYDRAULIC MODEL**

### <span id="page-27-4"></span>**3.1 Model extent**

[Figure 7](#page-28-0) displays the extent of the boundary of the hydraulic model. The extent of the boundary was defined this way due to the following criteria.

#### <span id="page-27-5"></span>*Available Elevation Data*  $3.1.1$

The feature that had the most influence on the hydraulic extent was the available lidar for this area. As discussed previously, the Vicmap DTM is not of a suitable resolution to be used for hydraulic modelling at this scale. The only elevation data that was used for the hydraulic modelling was the West Gippsland Riparian Lidar and the West Gippsland Floodplain Lidar datasets.

#### <span id="page-27-6"></span> $3.1.2$ *Grid Resolution*

Grid resolution is another typical constraint when defining the amount of area able to be modelled. The grid resolution needs to be fine enough to be able to adequately represent the significant waterways, while also having a model simulation time that can be ran within a reasonable timeframe.

Recommendation from TUFLOW is that in order to adequately represent the waterway, the grid resolution must be fine enough to allow at least 3-4 cells to fit across the waterway (BMT, 2018). The resolution of the elevation grid input into TUFLOW was 2 metres. Towards the upstream sections of the catchment the stream width varies between 3-4 metres, which is less than the acceptable levels.

#### <span id="page-27-7"></span> $313$ *Flood data*

After taking the above criteria into consideration, and performing some initial runs, the extent of the hydraulic model was refined further to remove section of the model that had not received any flooding. This was done to further reduce the run time of the model.



<span id="page-28-0"></span>**Figure 7 Hydraulic Model Extent**

### <span id="page-29-0"></span>**3.2 Input data**

#### <span id="page-29-1"></span> $3.2.1$ *Gridded elevation data*

Almost all the topography data input into TUFLOW was done using a Digital Elevation Model (DEM). As mentioned above, the DEM input into TUFLOW had a 2-metre resolution. The DEM was generated by resampling the West Gippsland Riparian Lidar Dataset from a 1-metre resolution to a 2-metre resolution. The resampling was performed within TUFLOW.

The resampling was necessary as to reduce the run time to a practical duration. The cell size still satisfies the recommendations from TUFLOW that the resolution should be fine enough to be able to fit 3 cells across the width of the river at the point of interest.

The digital elevation grid was altered using TUFLOW's zsh shapes and commands. The bridges had been removed from the Riparian dataset as part of its post processing and the zsh commands raised the elevation around the bridges to the equivalent height of the bridge deck.

#### <span id="page-29-2"></span> $322$ *Flow data*

As mentioned previously in this report, the flow hydrographs generated from RORB were input into the hydraulic model. The flow data was input into TUFLOW using either a 2D boundary condition line (2d\_bc\_L) or a 2D source area polygon (2D\_SA\_R), these shape files referenced flow vs time plots from external csv directed by the boundary condition data base (bc\_dbase).

2D\_bc\_Ls and 2D\_SA\_Rs were used based on whether or not the source of flow originated from inside or outside of the hydraulic boundary area. [Figure 8](#page-30-0) describes the locations of inflow into the hydraulic model.



<span id="page-30-0"></span>**Figure 8 Location of model inflows and outflows**

#### <span id="page-31-0"></span> $3.2.3$ *Materials*

The material layers and tables were used to define the Manning's roughness coefficients across the hydraulic model. The Manning's coefficients were varied spatially through the use of material shape files (shown in [Figure 9\)](#page-32-0). The model was divided up into 4 different material types, [Table 4](#page-31-1) displays the different material types and values used.

The digitisation of these material types was done primarily using the areal imagery, with the land use layers helping define residential and road materials.

![](_page_31_Picture_99.jpeg)

#### <span id="page-31-1"></span>**Table 4 Material Parameters**

![](_page_32_Figure_1.jpeg)

<span id="page-32-0"></span>**Figure 9 Material Layer**

### <span id="page-33-0"></span>**3.3 Assumptions**

#### <span id="page-33-1"></span>*Loss model*  $3.3.1$

Losses were modelled during the hydrology modelling stage, not within the hydraulic model. This means that all water that enters the hydraulic model will either exit the model through the outlet or remain in the model until the simulation finishes. This can cause water to remain trapped in small depressions in the model, potentially acting as an unintentional additional loss that was not accounted for during the hydrology modelling phase. However, the volume of water "lost" as a result of this is likely to be negligible.

#### <span id="page-33-2"></span> $3.3.2$ *Waterway delineation*

As mentioned previously, the assumptions made during the delineating of waterways as part of the hydrology phase has caused some minor flow paths into the main Eaglehawk Creek channel to be omitted. While this may result in some localised inundation around the edges of the model being missed, omitting these flow paths is unlikely to have a significant effect on the overall flood behaviour of the Traralgon Creek.

#### <span id="page-33-3"></span> $3.3.3$ *Flow application*

The applications of flow are defined in [Figure 9.](#page-32-0) Of particular concern is the internal flow sources which use Source Area polygons (2d SA) to define the location of runoff when the centroid of a subarea falls within the boundaries of the hydraulic model.

In reality, runoff would be spread out across the subarea, taking fine flow paths into the Traralgon Creek channel. Whereas the application of the flow using a SA polygon was restricted to often a 16 square metre area, typically placed directly within the main channel of the Eaglehawk Creek. This approach has the potential to artificially reduce the time that the catchment takes to convert runoff from rainfall and to miss possible flow paths. However, as shown by the hydrographs in [0,](#page-24-2) the amount of runoff produced by subareas with centroids within the hydraulic boundaries tend to be less significant.

#### <span id="page-33-4"></span> $3.3.4$ *Roughness model*

The roughness model used by the study applies a singular Manning's value to a particular material type. It is likely that the roughness of the catchment material would change due to factors like; the depth of flood waters, vegetation being flattened during larger events, and growth or removal of vegetation.

Additionally, the accuracy of the definition of material type is dependent largely on how the catchment has changed since the capture of the imagery datasets.

### <span id="page-33-5"></span>**3.4 Parameters and settings**

TUFLOWs HPC simulation mode uses an adaptive timestep.

#### <span id="page-33-6"></span>**3.5 Sensitivity analysis**

The hydraulic model was tested to see how sensitive it was to certain parameters. The parameters that were tested are as follows;

The Manning's roughness coefficient within the material csv. The Manning's coefficient was adjusted by ±20%.

The hydraulic slope of the downstream HQ boundary, which was also adjusted by  $\pm 20\%$ .

The changes to the parameters listed above have had little effect on the hydraulic results. The effect being changes in maximum velocity by less than ±0.3 m/s, maximum depth by less than  $\pm 0.1$  meters and maximum water surface elevations by less than  $\pm 0.1$  meters. These effects are slight when compared to the effect that the results from the hydrologic model have on the hydraulics in terms of hydrograph shape and peak flows and the uncertainty involved when producing these hydrographs.

### <span id="page-34-0"></span>**3.6 Results**

The results from this flood study are available in GIS form, located in a SDS compliant geodatabase.

The results feature raster datasets showing flood depths, velocities, water surface elevation and the digital terrain model used. In addition to the raster data, flood extent polygons and water surface elevation contours are also available.

Time series xmdf layers and animation videos are also available, which show the flood across time.

# <span id="page-35-0"></span>**SECTION D CONCLUSION AND RECOMMENDATIONS**

# <span id="page-35-1"></span>**1 CONCLUSION**

The Eaglehawk Creek floodplain mapping provides an analysis and review of existing and future potential flood risks along the areas around Glengarry.

Key outcomes from the study identify that the Eaglehawk catchment has a broad floodplain, which is prone to flooding to some degree during floods in all magnitude ARI events. Due to the land use of the catchment area being predominately farming, a large number of rural properties are subjected to flooding however minimal residential structures are likely to be impacted.

## <span id="page-36-0"></span>**SECTION E REFERENCES**

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